MTR Corporation Limited

TUEN MUN SOUTH EXTENSION

(No. EP-615/2022)

Rail Noise Mitigation Plan

		BM				
Certified by	:					
		(Raymond Wong)				
Position	:	Environmental Team Leader				
Date	:	19 April 2024				
Verified by	:	Ad-				
		(Adi Lee)				
Position	:	Independent Environmental Checker				
Date	:	19 April 2024				



MTR Corporation Limited

Consultancy Agreement No. C1502

Tuen Mun South Extension

Rail Noise Mitigation Plan

April 2024

	Name	Signature
Prepared & Checked:	Ben Wong	Beneti
Reviewed & Approved:	Angela Tong	Angel

Version:	6	Date:	18 April 2024
Consultancy Agreement N Corporation Limited without possession a copy of this R	lo. C1502 and may not be disclosed out our prior written consent. No	ed to, quoted to or relieve person (other than N port without our express	penefit in relation to and pursuant to d upon by any person other than MTR /TR Corporation Limited) into whose s written consent and MTR Corporation

AECOM Asia Co. Ltd. 12/F, Grand Central Plaza, Tower 2, 138 Shatin Rural Committee Road, Shatin, NT, Hong Kong Tel: (852) 3922 9000 Fax: (852) 3922 9797 www.aecom.com



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1 INTRODUCTION

1.1 Background

- 1.1.1 The Tuen Mun South Extension (TME) (hereinafter referred to as "the Project") is one of the seven recommended railway schemes in the Railway Development Strategy 2014 ("RDS-2014"). The Project will extend the Tuen Ma Line (TML), from Tuen Mun (TUM) Station southwards by about 2.4 km, terminating at a new station near Tuen Mun Ferry Pier (i.e. Tuen Mun South (TMS) Station) with an intermediate station at Tuen Mun Area 16 (i.e. A16 Station).
- 1.1.2 An Environmental Impact Assessment (EIA) study for the Project was conducted in accordance with EIA Study Brief No. ESB-332/2020. The EIA Report (Register No.: AEIAR-236/2022) were approved under the Environmental Impact Assessment Ordinance (EIAO), with an Environmental Permit (EP) granted on 18 August 2022 (EP No: EP-615/2022).
- 1.1.3 According to the EIA Report (Register No.: AEIAR-236/2022) (hereinafter referred to as "the approved EIA Report"), rail noise mitigation measures in the form of vertical noise barrier, semi-noise enclosure and noise enclosure were proposed to mitigate the potential noise exceedances at the NSRs located to the north of TMS Station (i.e. Tuen Mun Wu Hong Police Quarters), north and south of A16 Station (i.e. the planned A16 property development, Oi Tak House and Oi Lai House).
- 1.1.4 The construction works of the Project are tentatively scheduled to commence in Q4 2023. Pursuant to Conditions 2.15 of EP-615/2022, a Rail Noise Mitigation Plan (RNMP) shall be certified by the Environmental Team Leader (ETL) and verified by the Independent Environmental Checker (IEC) as conforming to the findings and recommendations of the EIA Report, and shall be submitted to the Director of Environmental Protection (DEP) for approval no later than 2 months before commencement of construction works of the Project. If there is any change to the rail noise mitigation measures in the approved RNMP, an updated RNMP shall be deposited with the DEP, no later than 1 month before the implementation of such change. The RNMP shall include the following details:
 - A review of the noise mitigation measures and demonstration of the rail noise performance requirements set out in the approved EIA Report will be met with the mitigation measures; and
 - Implementation schedule in table form to clearly list out the mitigation measures to be implemented, and the implementation party, location, timing, and environmental performance required for implementation of the mitigation measures.

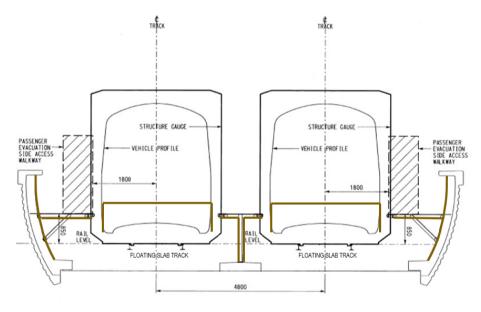
1.2 Purpose of this Plan

- 1.2.1 This RNMP presents the review findings of noise mitigation measures as recommended in the approved EIA Report and the implementation schedule with location of the rail noise mitigation measures.
- 1.2.2 In case of any change due to the rail operation and/or the design of the rail noise mitigation measures as well as any change to the assumptions/parameters that may affect the noise performance of the TME, the RNMP should be updated accordingly to demonstrate the compliance of noise requirement with updated implementation schedule of the proposed noise mitigation measures.

2 REVIEW OF RAIL NOISE MITIGATION MEASURES

2.1 Rail Noise Attenuation System

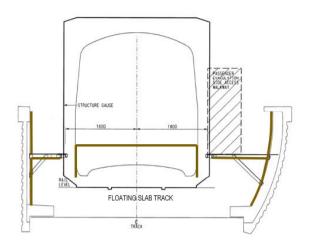
- 2.1.1 To minimize the potential rail noise from the Project, a multi-plenum noise attenuation system of Twin Track and Single Track (Diagram 2.1A and 2.1B refer), as proposed in the approved EIA Report, will be adopted for the Project. Detailed design of such attenuation system is described as follows.
 - Use of resilient rail base-plates for mounting tracks on viaduct to reduce vibration transmission to the viaduct structure, thereby reduce re-radiated noise from the viaduct structure;
 - Mounting of track on a floating slab system to further reduce vibration transmission to the viaduct structure;
 - Use of train skirts and floor with absorptive lining to create a noise-absorbing plenum beneath the train car. The train skirts would be extended to approximately 250mm above the derailment containment upstand on the floating slab in normal running;
 - Use of edge wall of about 1.2m above walkway with sound absorption to form an additional barrier for sensitive receivers at lower floor levels; and
 - Use of central plenum and trackside walkways (<=1.3m width) to create noiseabsorbing plena on both sides of the train car.



Sound Absorption Material

Diagram 2.1A Illustration of Multi-plenum System (Twin Track)





— Sound Absorption Material

Diagram 2.1B Illustration of Multi-plenum System (Single Track)

2.2 Proposed Rail Noise Mitigation Measures

- 2.2.1 Based on the latest design information provided by MTR, the rail operation and the alignment of the TME remains unchanged from the EIA study, and thus the train operation parameters including the vertical profile as indicated in Appendix 2.1 of the approved EIA Report and the assumption of TME adopted in the railway noise assessment of the approved EIA Report (**Appendix A** refers) remain valid.
- 2.2.2 The design of TME structures including the viaduct, A16 and TMS Stations is same as those presented in the EIA study, with illustration of the design at A16 and TMS Stations is presented in **Appendix B**. In addition, same as the design adopted in the EIA stage, the rail tracks and stabling tracks at A16 Station would be fitted with floating slab track and have no structural connection with the building structure of the planned development atop A16 Station, such that vibration transmission through structural elements of building to the planned NSRs¹ atop A16 Station is not anticipated. For the TMS Station, given that the southern end is the overrun section where would not have train movement during normal operation.
- 2.2.3 In view of the above, it is anticipated that the railway noise impact assessment findings in the approved EIA Report remain valid. Rail noise mitigation measures in the form of semi-enclosure, enclosure with opening and vertical noise barrier as proposed in the EIA Report would still be applicable in mitigating the noise exceedances predicted at some of the NSRs during night-time period. Details of the proposed rail noise mitigation measures are provided in **Table 2.1**, with their locations depicted in the **Figure Nos. C1502/C/TME/ACM/M52/112 114**.

Track Direction ⁽¹⁾	Chainage	Type of Noise Mitigation Measures ⁽²⁾	Length, m
Up	138+280 to 138+480	Semi-enclosure with vertical wall on East Side and open on West side. Roof shall extend up to the car body edge of Down track.	200
Up	138+520 to	Semi-enclosure with vertical wall on East side	75

Table 2.1	Recommended Rail Noise Mitigation Measures
	Robolinnenada Ran Holde mitigation medeado

¹ Design and planning parameters of A16 development, i.e. the development boundary of the planned A16 development shown in Figure C1502/C/TME/ACM/M52/113, Footnote [6], [7] and [11] of Table 4.6 of the EIA Report remain valid.



Track Direction ⁽¹⁾	Chainage	Type of Noise Mitigation Measures ⁽²⁾	Length, m
	138+595	and open on West side. Roof shall cover both Up Track, siding and turnout.	
Up	138+595 to 138+682	Semi-enclosure with vertical wall on East side of siding track and open on West side of Up Track. Roof shall cover siding track and shall extend up to the car body edge of Up Track.	87
Up	138+981 to 139+060	Semi-enclosure start from South end of A16 Station with vertical wall on East side and open on West side. Roof shall cover whole Up Track.	79
Up	139+060 to 139+163	Semi-enclosure with vertical wall on East Side and open on West side. Roof shall cover both Up Track, Down Track, siding and turnout.	103
Up	139+582 to 139+722	Noise Enclosure with 2m wide opening at the	140
Down	139+585 to 139+725	middle of the roof	140
Up	139+722 to 139+832	1m high noise barrier above exterior parapet (i.e. 3.1m above top of rail) on East side which shall extend to North end of TMS Station platform	110
Down	139+725 to 139+836	1.5m high noise barrier above exterior parapet (i.e. 3.6m above top of rail) on West side which shall extend to North end of TMS Station platform	111

Notes:

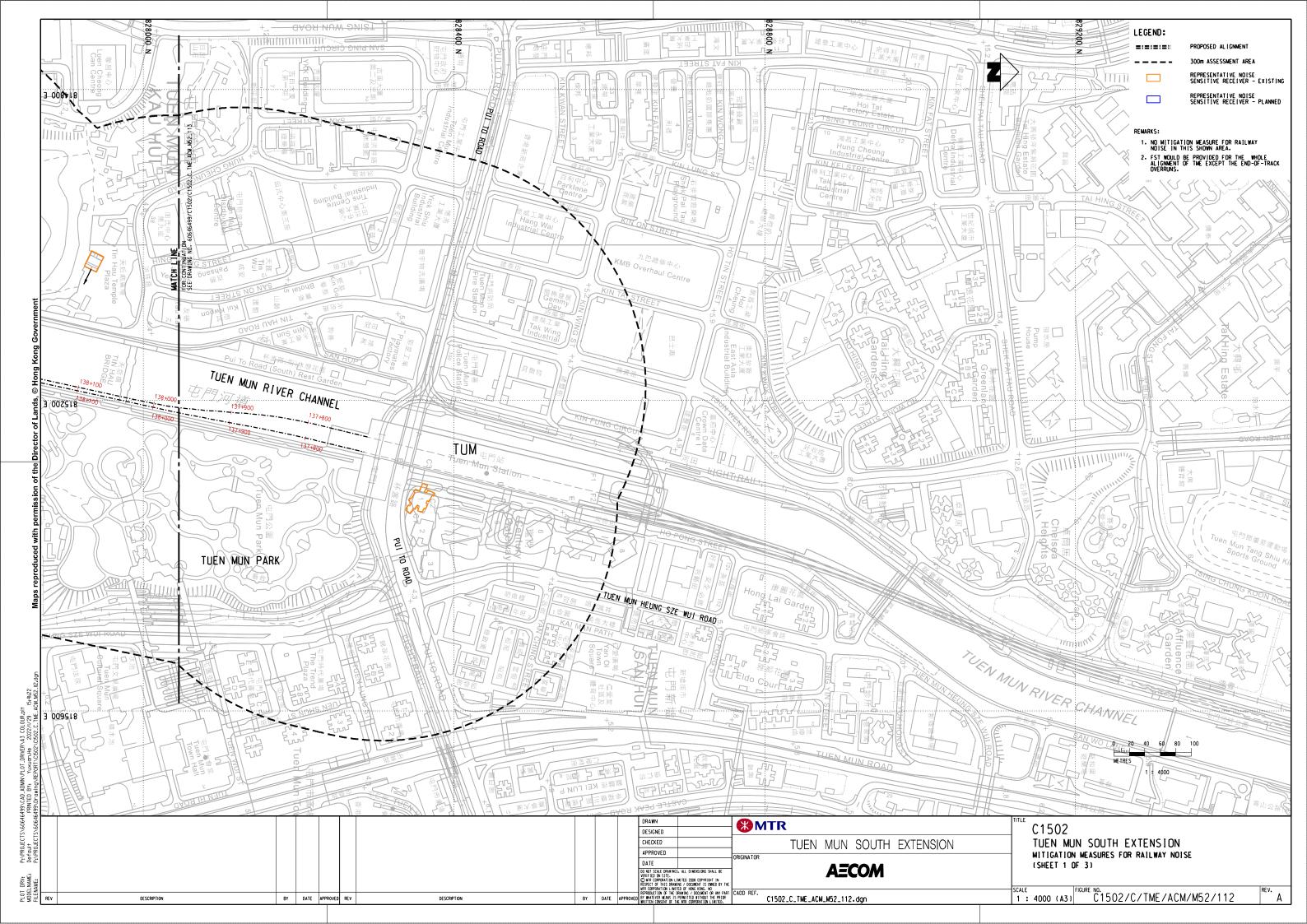
(1) Up track - train direction to Tuen Mun South Station; Down track - train direction to Tuen Mun Station.

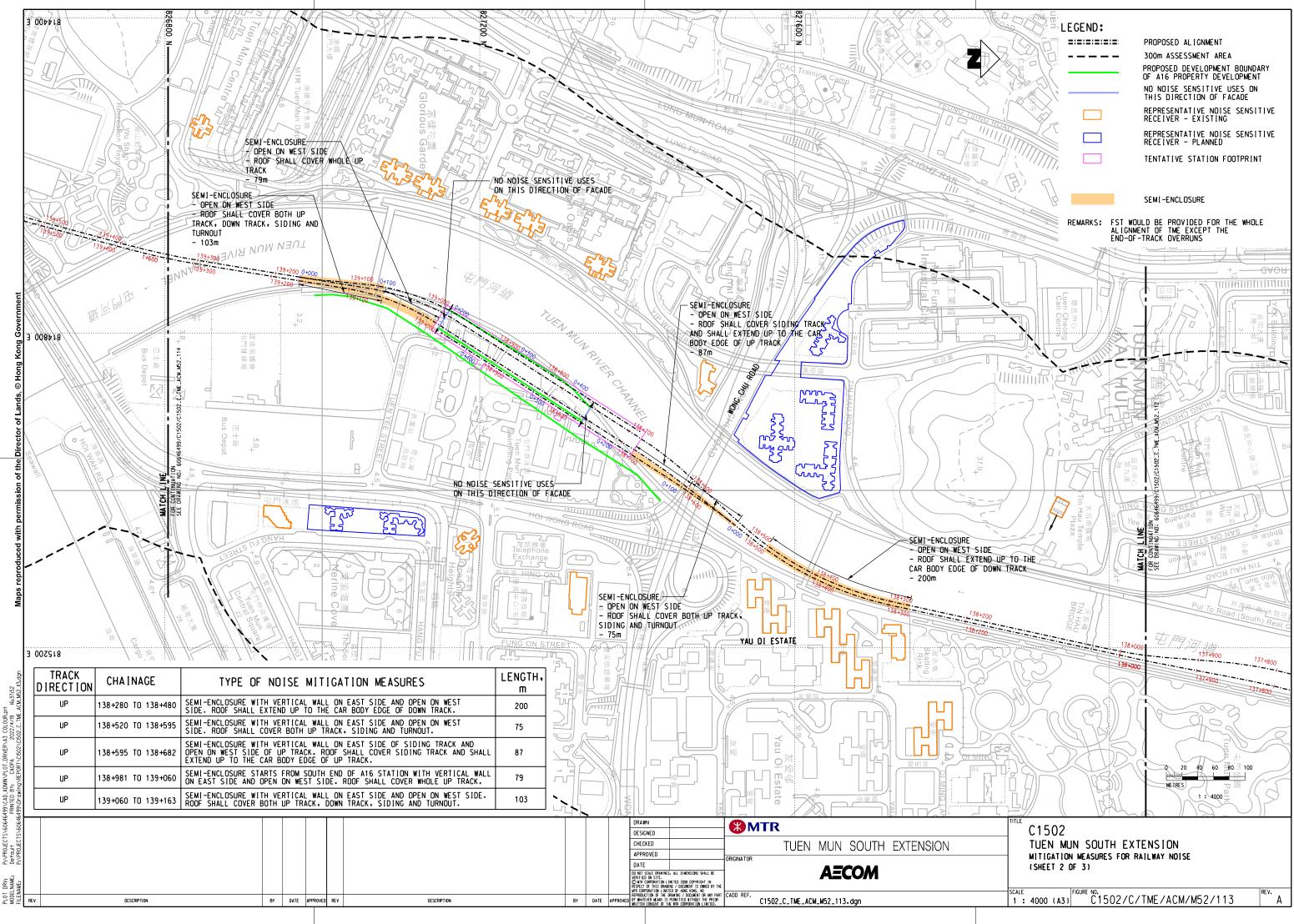
(2) The height of the semi-enclosure/enclosure is about 6m on top of 1.2m edge wall of viaduct subject to detailed design.

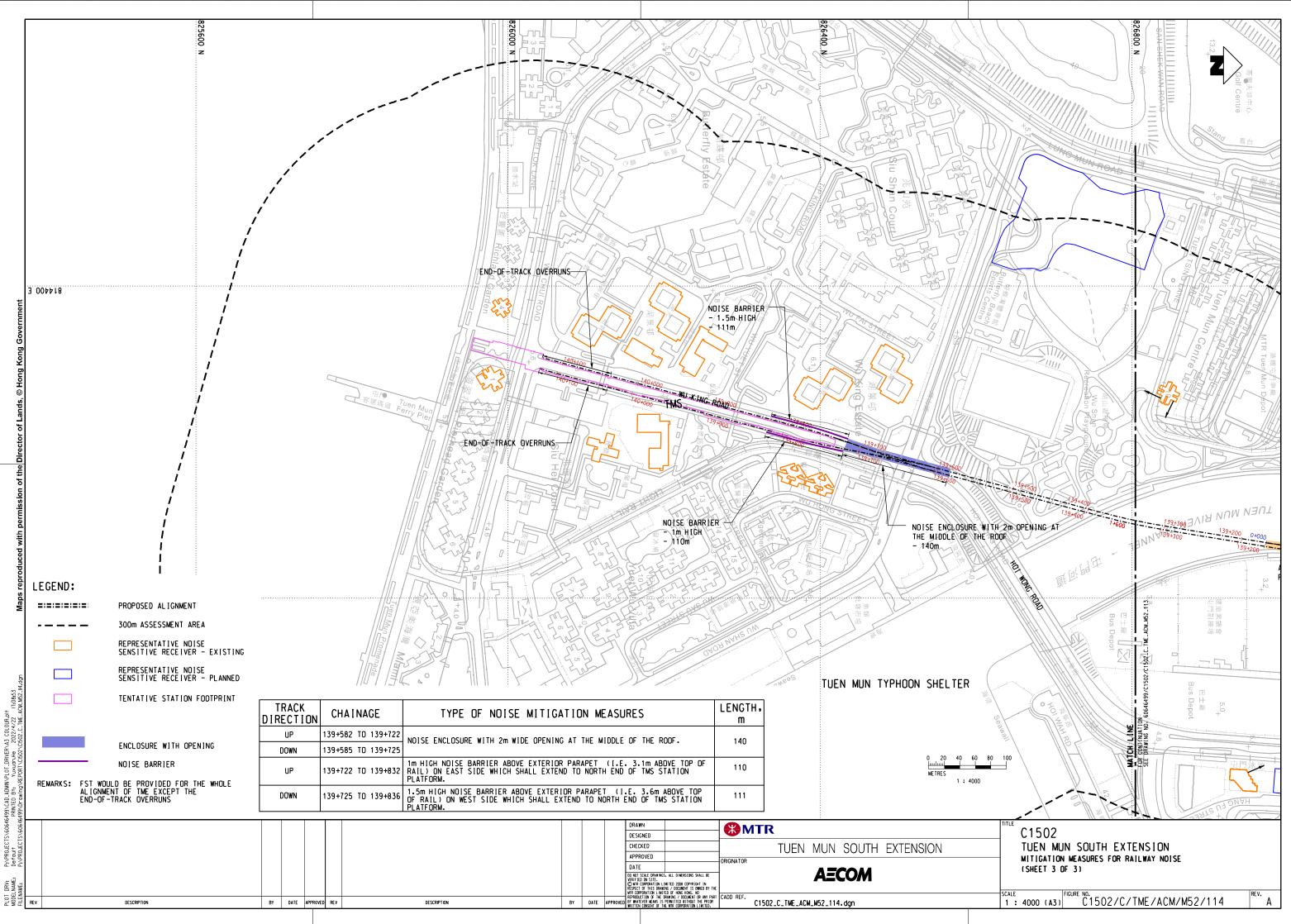
- 2.2.4 To reduce the sound reflection and portal effect arising from the installation of rail noise mitigation measures, internal surface of the proposed noise barriers, semi-enclosure and noise enclosure with opening would be equipped with acoustic panel or sound absorption lining.
- 2.2.5 With the implementation of the proposed rail noise mitigation measures provide in **Table 2.1**, both predicted rail noise operation of the Project and the cumulative rail noise impact would comply with the rail noise performance requirements set out in the approved EIA Report.
- 2.2.6 The implementation schedule of the proposed rail noise mitigation measures is provided in **Appendix C**.



Figures









Appendix A

Assessment Assumptions and Operation Parameters

Assumptions Adopted in Railway Noise Assessment

Item	Parameters			
Train Type and No. of Car	Electric Multiple Unit train, train length 200m for 8-car train			
Train Source Term ⁽¹⁾ for 8-car train at 130kph at 25m Train Frequency per hour per Direction	 SEL = 81.4 dB(A) ⁽²⁾ Structure Re-radiated Noise: Typical Viaduct, Plain Track – Leq, 30min = 40.6 dB(A) Viaduct, turn out inside enclosure – Leq,30min = 47.1 dB(A) Air-Conditioning Noise: Lmax = 48.8 dB(A) (at viaduct for running train) Lmax = 54.8 dB(A) (at station for running train) SWL = 83.5 dB(A) (at station for each Airconditioning unit of stationary train) Mainline⁽³⁾: 28 number during peak daytime period (0700 – 2300 			
	 hours) 20 number during peak night-time period (2300 – 0700 hours) Sidings⁽⁴⁾: 2 number during daytime and night-time periods 			
Gap Size ⁽⁵⁾ Correction	+10 log(G/250)			
Speed Correction	 Speed Profile⁽⁶⁾ of TME is provided in <u>Appendix 4.15B</u>. 20 log10 (V/Vref) where V = Train speed, Vref = Reference train speed 			
Train Frequency Correction	+10 log10 (N) where N = Train frequency per 30 min per Direction			
Distance Correction	Cdist = $-10 \log_{10}$ (dist/25) where dist is the perpendicular slant distance of track segment to NSR in meters			
Screen Correction	As per CRN Chart 6(a) & Chart 6(c)			
Angle of View Correction	Cangl = 10 log ₁₀ [$\pi\theta/180 - \cos 2\alpha \sin \theta$] – 5 where θ is angle subtended by the segment at NSR, and α is orientation of the segment along the trajectory of the track <i>Ref: CRN Chart 7</i>			
Air Absorption Correction	Cair = 0.2 – 0.008 x d' (where dist is slant distance from track to NSR) <i>Ref: CRN Chart 4</i>			
Reflection Correction	Ref: CRN Chart 4 Crefl = 1.5 (θ'/θ) dB(A) (θ' is the sum of the angles subtended by all reflecting facades on the opposite side of the railway facing the receiver point and θ is the total angle subtended by the source line at the receiver point, +1.5dB maximum correction for each reflection Ref: CRN Clause 31.2)			

Item	Parameters
Façade Correction	+2.5 dB(A)
Rail and Rolling Stock Condition Deterioration	+3 dB(A)
Joint/Turnout Correction	+7 dB(A)

Notes:

- (1) Considering that the design of TME would adopt same design configuration of the WRL, i.e. floating slab track (FST) for minimisation of structural-borne noise, and a multi-plenum system which includes (1) an undercar sound-absorbing plenum formed by vehicle side skirts; (2) "underwalkway" sound-absorbing plena on both sides of vehicle; and (3) edge walls with sound absorption for minimisation of air-borne noise, the source term as adopted in West Rail Operation Noise Assessment Report (July 2015) would be applicable to the rail noise assessment of TME.
- (2) According to rolling noise source term adopted in West Rail Operation Noise Assessment Report (July 2015), SEL of 8-car train at 130 kph at 25m for down track (to Hung Hom) and up track (to Tuen Mun) are 81.4 dB(A) and 80.7 dB(A) respectively. As a conservative approach, SEL of 81.4 dB(A) was adopted for rail noise assessment. Reference was also made on West Rail Operation Noise Assessment Report (July 2015) for the source term of structure re-radiated noise and A/C noise.
- (3) Train frequency of the Project follows the current train frequency of WRL and are same as those adopted in West Rail Operation Noise Assessment Report (July 2015). The 30-minute train movement will be 50% of the hourly movements provided.
- (4) There will only be a maximum of 1 number of siding train per 30 minutes during day-time, evening and night-time periods and the multi-plenum system will be provided on the viaduct of the stabling sidings.
- (5) The standard gap size between the train and walkway of TME is 250mm at the plain track and up to about 400mm at the curve track area. Following the same assessment approach as adopted in WRL, a correction factor of +10 log(G/250) was included in the calculation according to the identified gap size location larger than 250mm.
- (6) Train speed will be controlled by automatic signal control system and thus the trains running on TME will be operated according to the train speed profile.

Remark:

SEL = Lmax + 10log(L/V) +10.5 - 10log[(4D/(4D2+1)) + 2tan-1(1/(2D))]

where D = d/L, d = perpendicular distance from the track (m), L = train length (m) and V = train speed (km per hour)

Modelling Assumptions and Calculation Methodology

Item	Details of Assumptions/Methodology				
Modelling Assumptions	•	Rolling Noise: At 0.9m above top of rail level			
	•	Structure Re-radiated Noise : At 1m below top of rail level and 1m away from parapet wall horizontally			
	•	Air-Conditioning Noise: At 4m above top of rail level ⁽¹⁾			
	•	Rolling Noise through vent at A16 Station: SWL of 53.5 dB(A) per unit area			
	•	Air-Conditioning Noise from stationary train at TMS Station: Time factor of $50\%^{(2)}$ (with trains swap to park in each platform in turn, and thus stationary train will stay about 50% of time)			
	•	Openings of the sidings at A16 Station: 1.5m in height			
	•	Operation mode within sidings: Train will not idle in the sidings (i.e. train will be shut down after arrival / will be started only before launching to mainline)			
	•	At least 50% of the sidewall of the sidings provided with acoustic panel with a minimum absorptive coefficient of 0.7.			
	•	Mainline completely segregated from the sidings with solid walls such that the noise from the mainline will not break out via the openings of the sidings			
	•	Maximum train speed within sidings limited to 25kph			
	•	Ceiling roof of TMS Station with acoustic panels			
	•	Building structure of about 23.4mPD at both ends of TMS Station			
Calculation Methodology	•	Rolling Noise (Line Source): CRN ⁽³⁾			
	•	Structure Re-radiated Noise (Line Source): CRN ⁽³⁾			
	•	Air-Conditioning Noise for running train (Line Source): CRN ⁽³⁾			
	•	Air-Conditioning Noise for stationary train (Point Source): ISO 9613			
	•	Rolling Noise through vent at A16 station, Area Source ⁽⁴⁾ : ISO 9613			
	•	Gap Size Correction: +10 log(G/250)			
	•	Speed Correction: 20 log10 (V/Vref) where V = Train speed, Vref = Reference train speed			
	•	Train Frequency Correction: +10 log10 (N) where N = Train frequency per 30 min per Direction			
	•	Distance Correction (CRN): Cdist = $-10 \log 10$ (dist/25) where dist is the perpendicular slant distance of track segment to NSR in meters			
	•	Screen Correction: CRN Chart 6(a) & Chart 6(c)			
	•	Angle of View Correction: Cangl = 10 log ₁₀ [$\pi\theta$ /180 – cos 2 α sin θ] – 5 where θ is angle subtended by the segment at NSR, and α is orientation of the segment along the trajectory of the track (Ref: CRN Chart 7)			
	•	Air Absorption Correction: Cair = $0.2 - 0.008 \text{ x}$ d' where dist is slant distance from track to NSR (Ref: CRN Chart 4)			

Item	Details of	Assur	nptions/I	Methodol	ogy			
	angles the rail subten correct	angles subtended by all reflecting facades on the opposite side of the railway facing the receiver point and θ is the total angle subtended by the source line at the receiver point, +1.5dB maximum correction for each reflection (Ref: CRN Clause 31.2)						
	Rail an	d Rolli	ng Stock	Condition	Deteriorat	ion: +3 dB((A)	
	 Joint/T 	urnout	Correctio	on: +7 dB(A)			
Gap Size			TML CI	hainage	Outside Curve	Inside Curve		
	Alignmnet	Curve No.	Start	End	Hori. Distance between Train Floor and Walkway (mm)	Hori. Distance between Train Floor and Walkway (mm)		
	Up Track	1	137+776.121	137+874.997	286	270		
		2	137+924.729	138+004.944	279	263		
		3	138+274.444 138+585.560	138+513.017 138+690.664	368 332	330 300		
	A16-STATION	-	100-000.000	100-000.004	332			
		5	138+969.066	139+116.175	400	380		
	TURNOUT	6	139+265.977	139+412.218	318	282		
	TURNOUT	7	139+667.577 139+716.485	139+702.562 139+778.994	336 315	336 315		
	TMS-STATION	, , , , , , , , , , , , , , , , , , ,	133-110.403	100-110.004	515	515		
	Dn Track	1	137+774.245	137+895.503	358	326		
		2	137+920.548	138+032.236	351	317		
		3	138+274.812	138+545.449	367	333		
	A16-STATION	4	138+585.648	138+698.869	371	339		
		5	138+942.868	139+089.978	400	380		
		6	139+270.410	139+415.994	319	281		
	TURNOUT	7	139+671.438	139+706.423	336	336		
	TMS-STATION	8	139+720.346	139+782.855	315	315		
	Dn Track TURNOUT	1	0+000.493	0+035.478	336	336		
	TORNOOT	2	0+061.671	0+035.478	390	390		
	Up Track							
	TURNOUT	1	0+000.493 0+053.242	0+035.478 0+113.647	336 278	336 278		
		2	07003.242	0+113.047	210	210		

Notes:

(1) There would be 2 A/C units at the roof of each car. For a 8-car train, there would be a total of 16 A/C units.
(2) The assumption of time factor (i.e. 50%) of Air-Conditioning Noise from stationary train at TMS station is based on worst-(2) case scenario as confirmed by the MTRC. The train source term adopted in this noise assessment was made reference from the noise measurement for the existing

(3) viaduct of West Rail. Given that the Project would adopt same multi-plenum system, the corrections for slab-track, bridges and viaduct, and ballast would not be required.(4) Prediction of noise emission from the openings is provided in Appendix 4.15A-1

A16 Siding Train Noise Emission from Openings

	-	0		
No. of Car	n	8		
Train	L	200		
Length (m)				
Ref. Train		100		
Speed	Vr	130		
(km/h)				
Ref.				
Setback	D	25		
Distance	_			
(m)				
Ref. SEL	SELr	81.4		
(dBA)	0221	01.1		
Train				
Speed	V	25		
(km/h)				
Track wear	0			
correction	Cw	3		
	SEL=SELr+			
SEL (dBA)	20*LOG(V/	70.1		
	Vr)+Cw			
No. of	N	1		
passby	0.01			
SPL	SPL = SEL-			
Leg,30min	10*log(30*6	37.5		
(dBA)	0)+10*log(N			
. ,)			
Line	Lw' =			
	SPL+8+10*I			
power	og(D)-	55.7		
density	10*log(2*ata			
(dBA)	n(L/2D))			
Line				
source				
	Lw'+10*log(78.7			
whole train	L)			
(dBA)				

Ref: Transportation Noise Reference Book equation 2.19

SPL of Train in Siding

Siding	Room	Internal	Dimension
--------	------	----------	-----------

	Length L	Width W	Height H
m	300	6.4	7

Absorption coefficient

/ aboon priori	000111010111		
	Concrete		Acoustic
Material	Finishes	Open End	Panel
α	0.02	1.00	0.70

Internal walls inside the siding

	Side	Wall		Open Er	nd at Exit	Closed I	End Wall	Cei	ling	Fle	oor
S	α	S	α	S	α	S	α	S	α	S	α
LxH		LxH		WxH		WxH		LxW		LxW	
	50%		50%								
	Concrete		Acoustic				Concrete		Concrete		Concrete
sq.m	Finishes	sq.m	Panel	sq.m	Open End	sq.m	Finishes	sq.m	Finishes	sq.m	Finishes
1050.0	0.02	1050.0	0.70	44.8	1.00	44.8	0.02	1920.0	0.02	1920.0	0.02

	Room Ab	osorption	
Total S	Total Sα	Average α	R
sq feet			
8129.6	1634.5	0.201	2045.8

		SPL of
Distance to		Train in
Opening	Directivity	Siding
r	Q	Lp
m		dBA
6	4	53.5

Ref Formula: general equation for calculating sound pressure from sound power in reverberant room. Lp=Lw+10log(Q/(pi*r*L)+4/R)

SWL for One Train at Opening of Siding

			SWL at	SWL per unit area at
Length	Height	S	opening	opening
L	Н	LxH		
m	m	sq m	dBA	dBA/sq.m
200	1.5	300.0	78.2	53.5

	CadnaA
	Input of
	SWL per
Facade	unit area at
Correction	opening
dB	dBA/sq.m
2.5	56.0

Legend: Lw: Sound Power Level dB re 10-12 W

Lw: Sound Power Level dB re 10-12 W

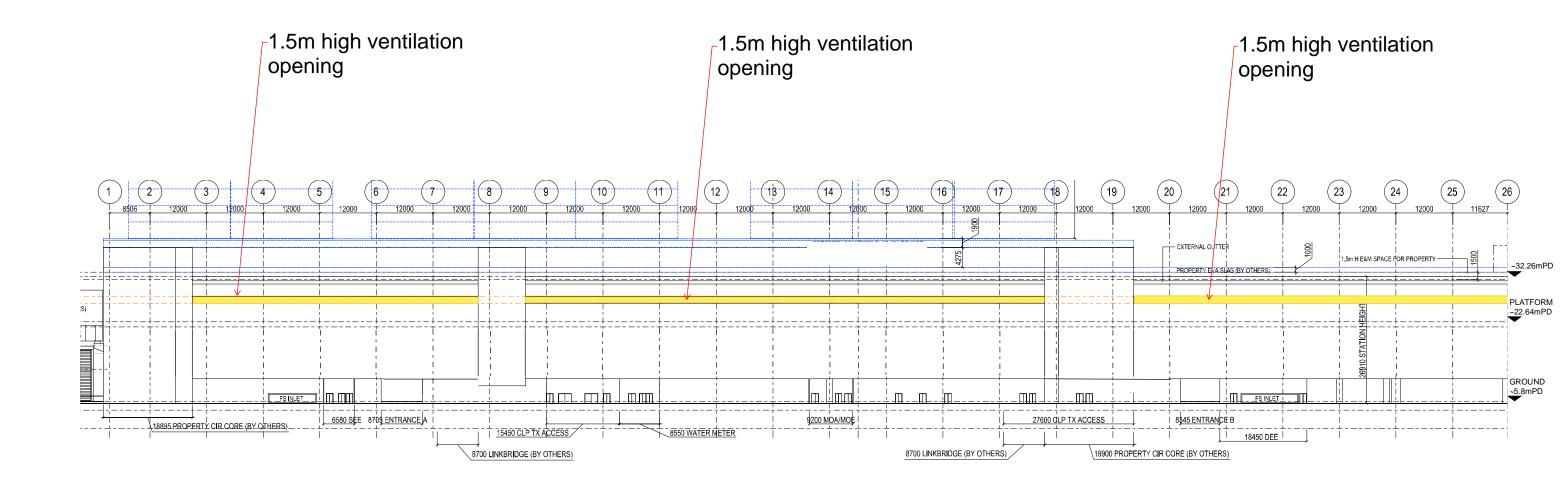
SPL (or Lp): Sound Pressure Level dB re 20μ Pa α : Absorption coefficient of wall/ceiling/opening

S: Surface area

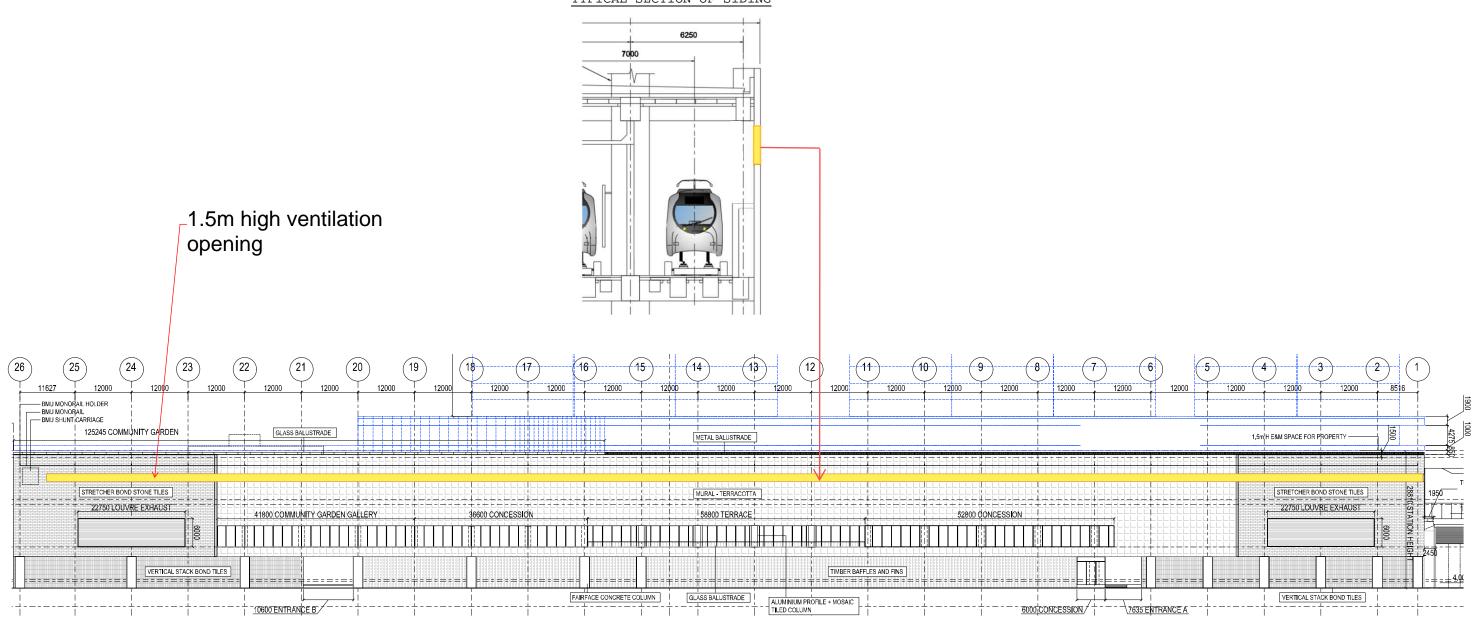
R: Room constant

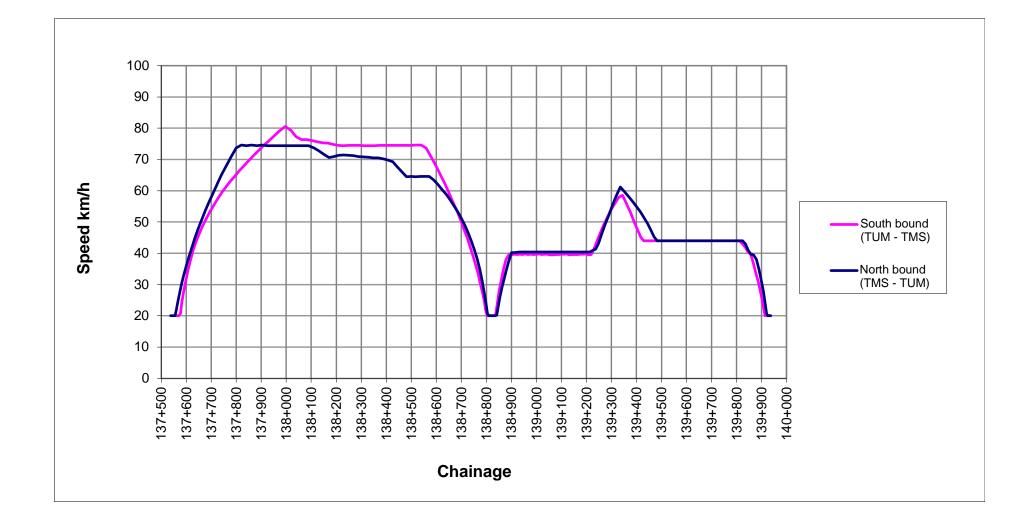
r: Setback from train inside the siding to opening

Q: Directivity factor



TYPICAL SECTION OF SIDING

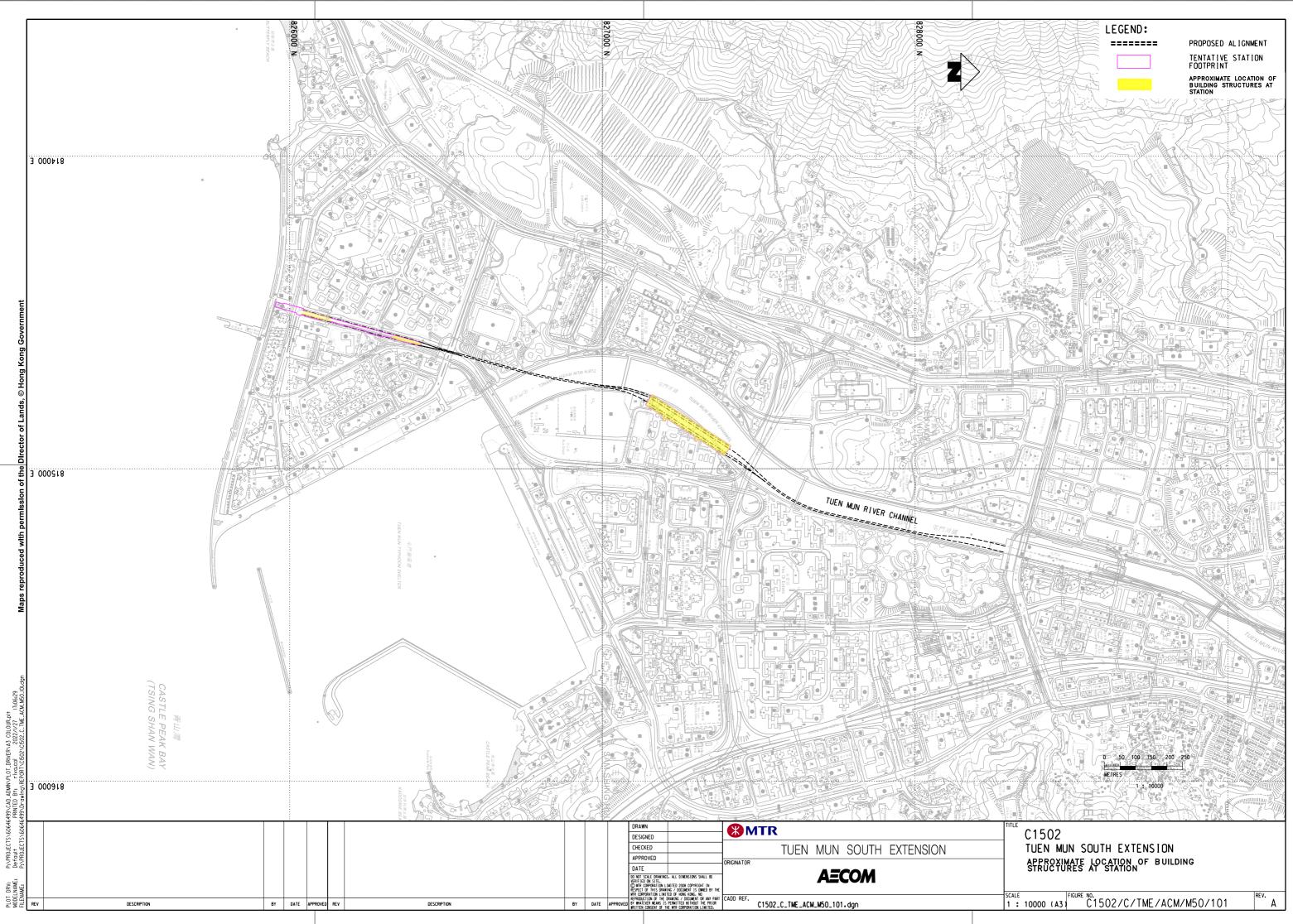


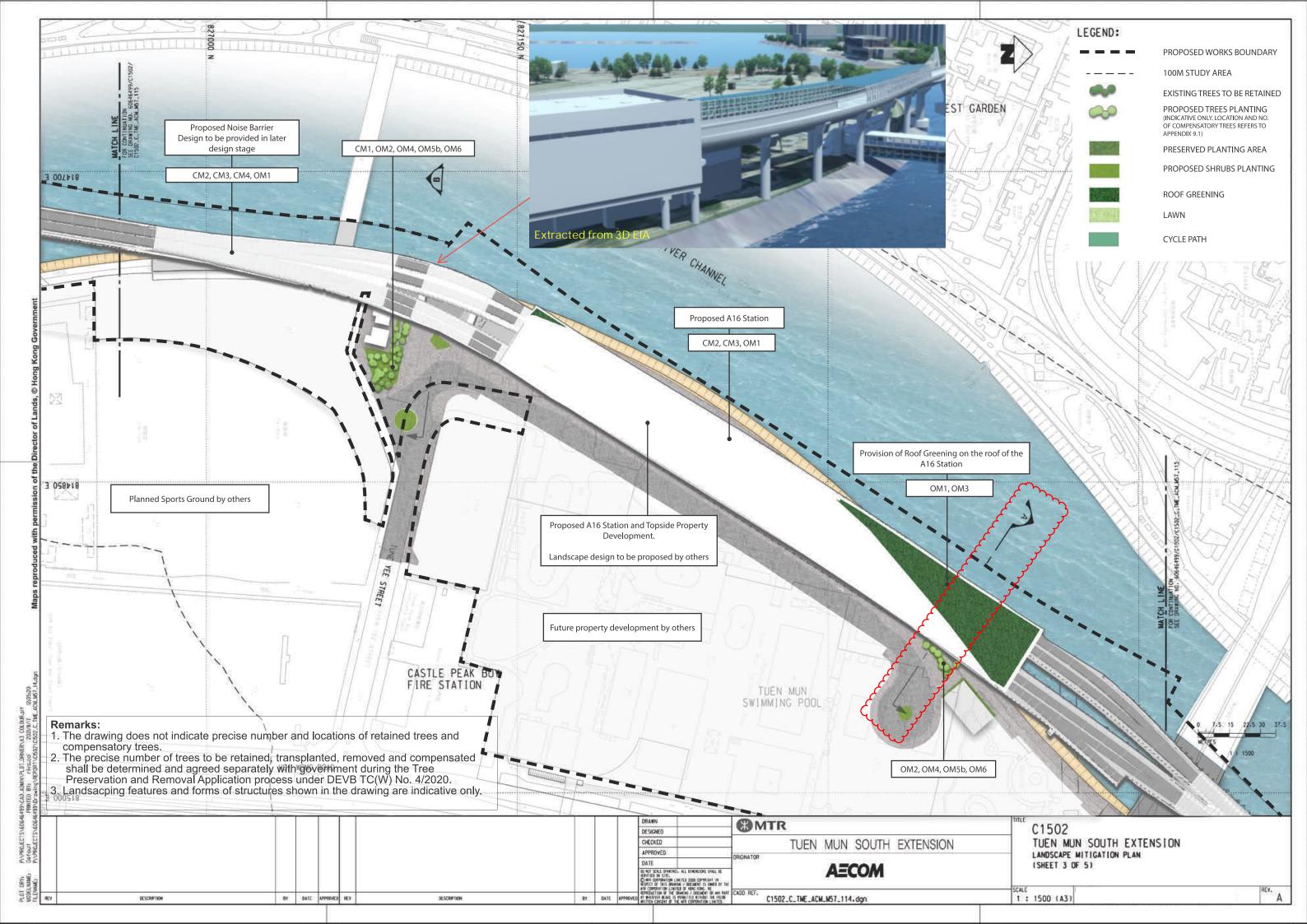


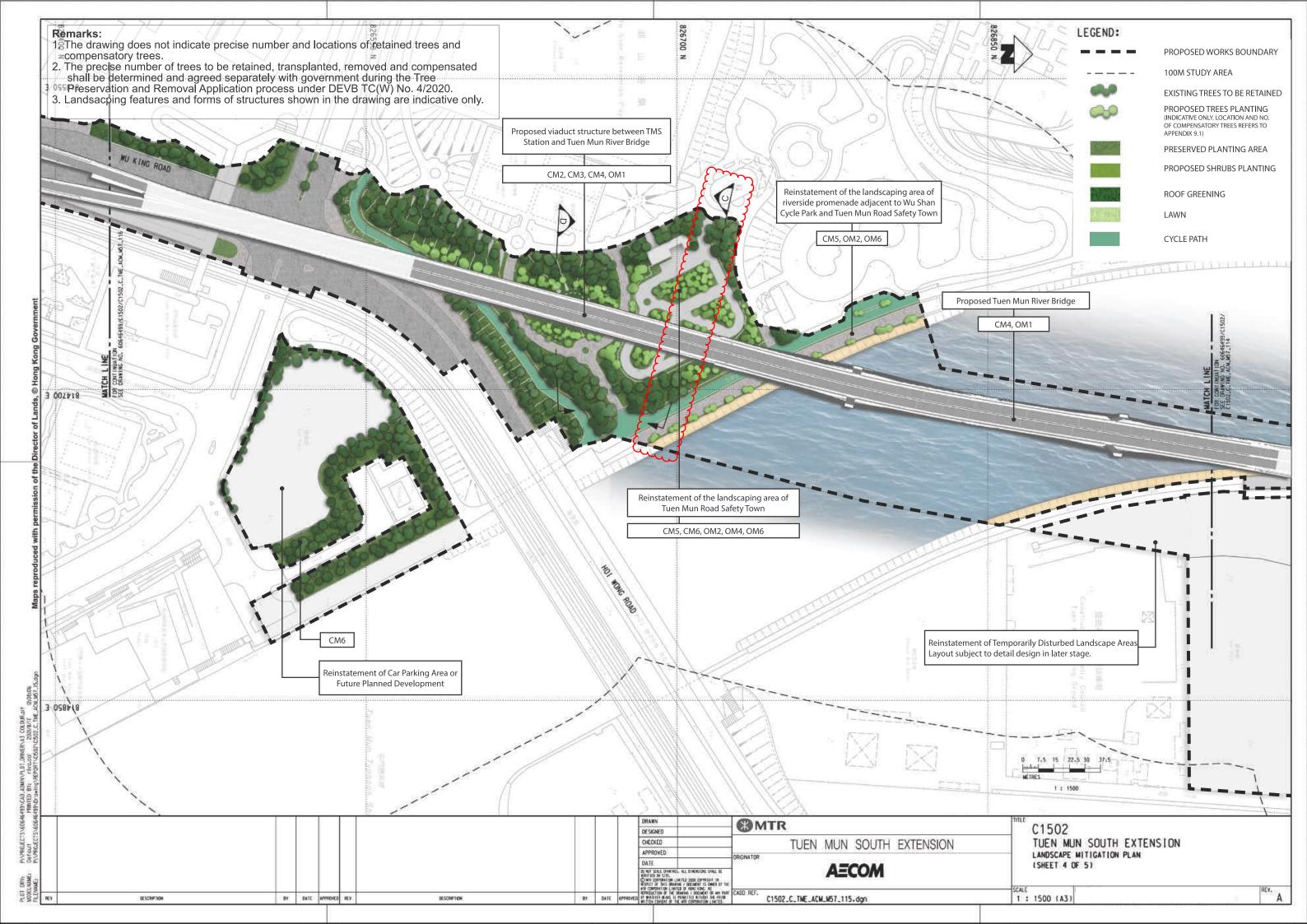


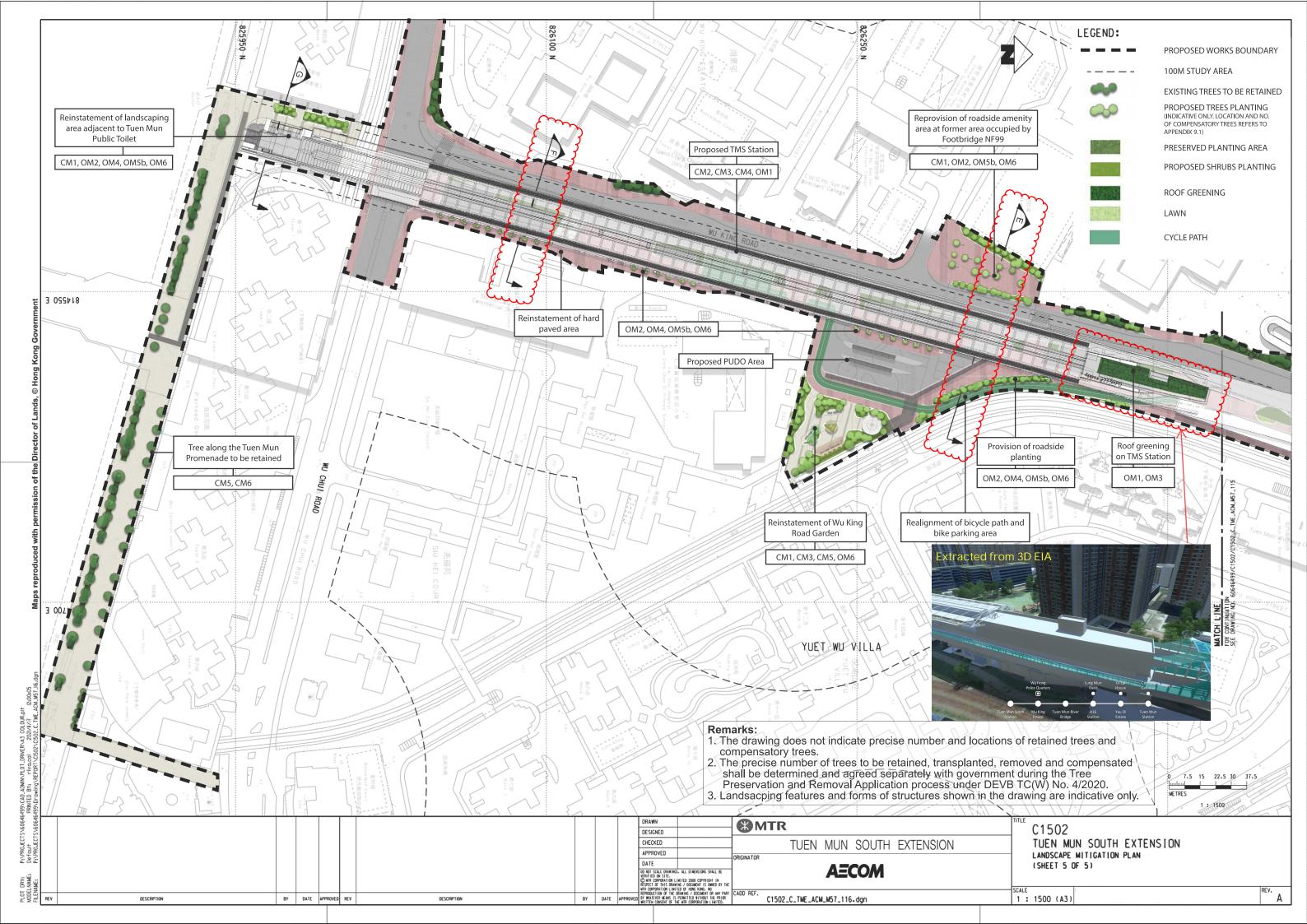
Appendix B

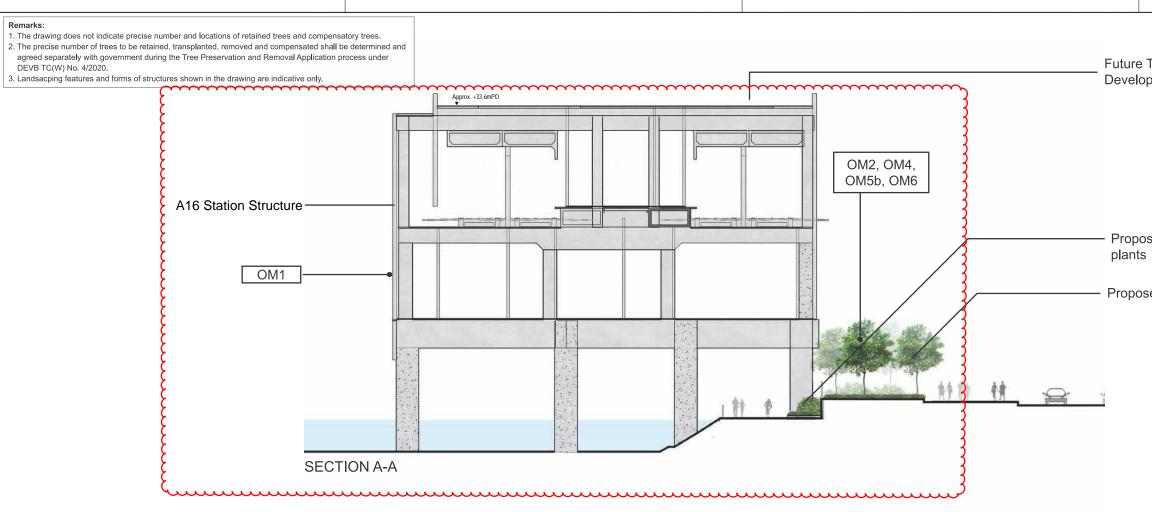
Design of TME Structures (For Illustrative Purpose)









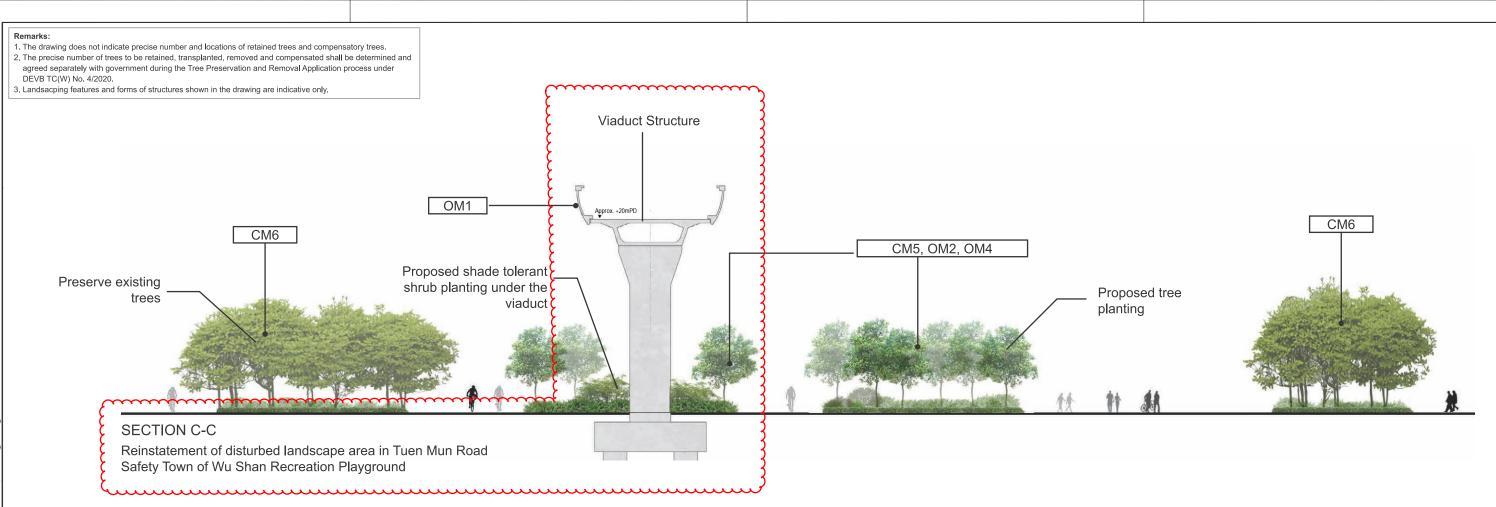


PAPROJECTS/60646499/CAD.ADM Defout PAPROJECTS/60646499/Chrowing		 DRAWN DE SIGN CHECKI	NED	TUEN MA EXTENSION	TUEN MUN SOUTH EXTENSION
636		APPRO	OVED ORIGINATOR	AECOM	IMPLEMENTATION OF MITIGATION MEASURES - SECTION (SHEET 1 OF 4)

Future Topside Property Development by others

Proposed shade tolerant

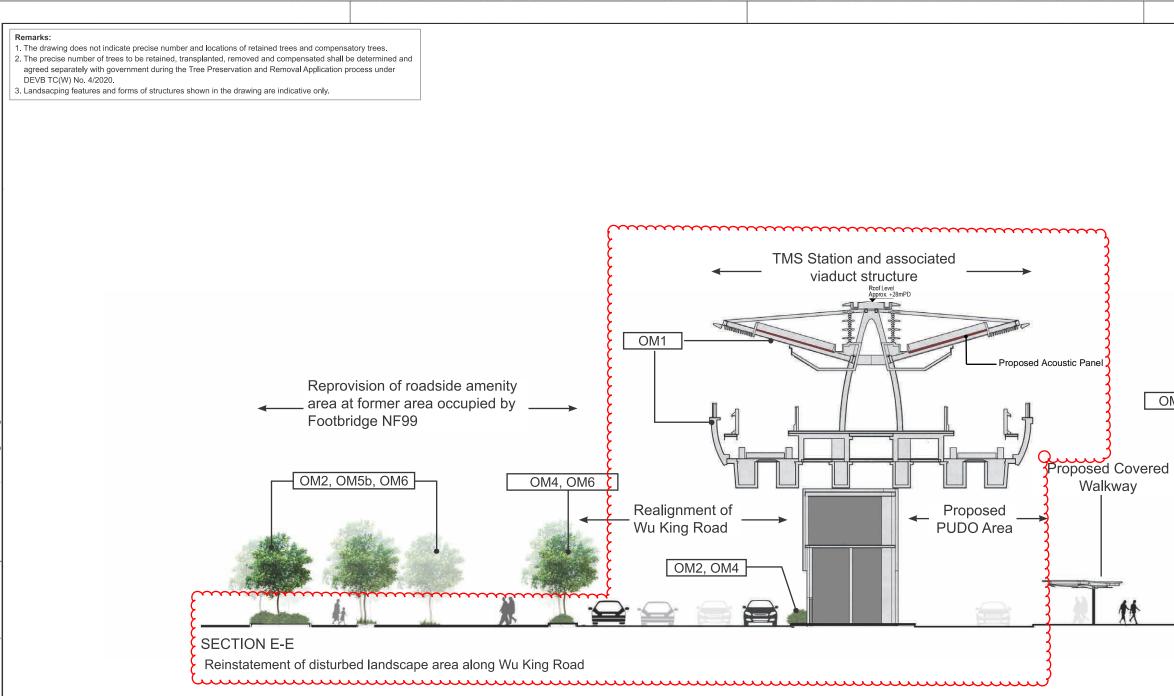
Proposed planting area



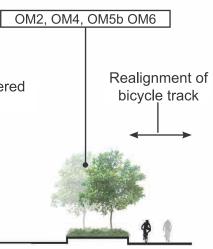
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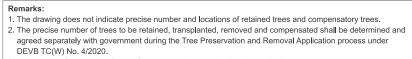
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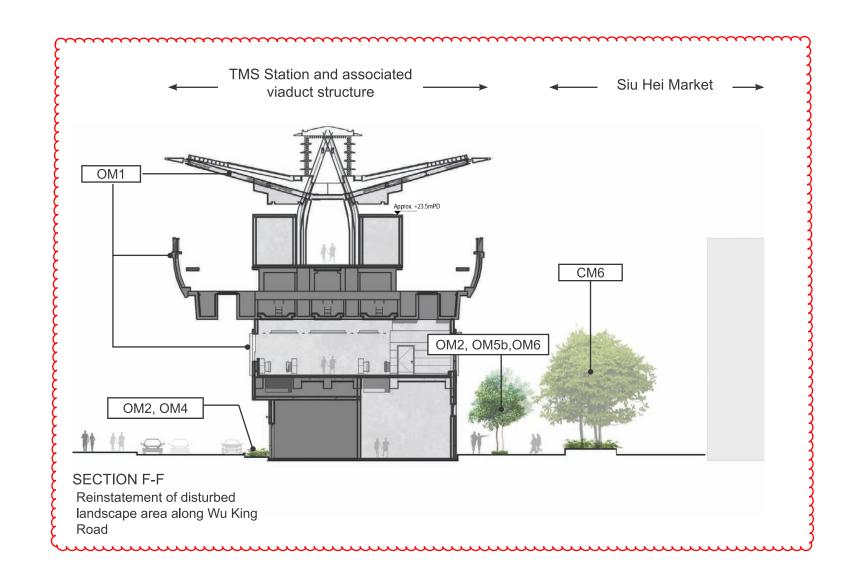


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3. Landsacping features and forms of structures shown in the drawing are indicative only.



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Appendix C

Implementation Schedule of the Rail Noise Mitigation Measures

Requirements

or Standard

to be achieved

EIAO-TM Annex 5 &

Noise Control

Reference Section in the RNMP	Recommended Rail Noise Mitigation	Implemented by		Tentative		
	Measures		Track Direction	From	То	- Construction Programme
Section 2.1.1	 Use of resilient rail base-plates for mounting tracks on viaduct to reduce vibration transmission to the viaduct structure, thereby reduce re-radiated noise from the viaduct structure; Mounting of track on a floating slab system to further reduce vibration transmission to the viaduct structure; Use of train skirts and floor with absorptive lining to create a noise- absorbing plenum beneath the train car. The train skirts would be extended to approximately 250mm above the derailment containment upstand on the floating slab in normal running; Use of edge wall of about 1.2m above walkway with sound absorption to form an additional barrier for sensitive receivers at lower floor levels; and 	MTRC		Along the TME	Ξ	Jul 2025 – Dec 2028

Implementation Schedule of Rail Noise Mitigation Measures

	 derailment containment upstand on the floating slab in normal running; Use of edge wall of about 1.2m above walkway with sound absorption to form an additional barrier for sensitive receivers at lower floor levels; and Use of central plenum and trackside walkways (<=1.3m width) to create noise-absorbing plena on both sides of the train car. 						Ordinance
Table 2.1	 Semi-enclosure⁽¹⁾ (Length:200m) with vertical wall on East Side and open on West side. Roof shall extend up to the car body edge of Down track 	MTRC	Up	138+280	138+480	Jul 2025 –	EIAO-TM Annex 5 &
	 Semi-enclosure⁽¹⁾ (Length:75m) with vertical wall on East side and open on West side. Roof shall cover both Up Track, siding and turnout 		Up	138+520	138+595	Feb 2028	Noise Control Ordinance

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Reference Section in the RNMP	Recommended Rail Noise Mitigation Measures	<u>}</u>	Location			Tentative Construction	Requirements or Standard
			Track Direction	From	То	Programme	to be achieved
	Semi-enclosure ⁽¹⁾ (Length:87m) with vertical wall on East side of siding track and open on West side of Up Track. Roof shall cover siding track and shall extend up to the car body edge of Up Track.		Up	138+595	138+682		
	• Semi-enclosure ⁽¹⁾ (Length:79m) starting from South end of A16 Station with vertical wall on East side and open on West side. Roof shall cover whole Up Track.		Up	138+981	139+060		
	• Semi-enclosure ⁽¹⁾ (Length: 103) with vertical wall on East Side and open on West side. Roof shall cover both Up Track, Down Track, siding and turnout.		Up	139+060	139+163		
	• Noise Enclosure ⁽¹⁾ (Length: 140m) with		Up	139+582	139+722		
	2m wide opening at the middle of the roof		Down	139+585	139+725		
	1m high noise barrier ⁽¹⁾ above exterior parapet (i.e. 3.1m above top of rail) (Length: 110m) on East side which shall extend to North end of TMS Station platform		Up	139+722	139+832		
	1.5m high noise barrier ⁽¹⁾ above exterior parapet (i.e. 3.6m above top of rail) (Length:111m) on West side which shall extend to North end of TMS Station platform		Down	139+725	139+836		

Note:

(1) The internal surface of the proposed noise barriers, semi-enclosure and noise enclosure with opening should be equipped with acoustic panel or sound absorption lining.