Particle modelling of pollutant dispersion from the new Kwun Tong nullah – Scenario 1C

- 1 A 2D particle model is used to model the pollutant dilution and dispersion in Victoria Harbour near the outfall of the new Kwun Tong Nullah. A conservative pollutant, i.e. without the incorporation of decay factor, is discharged at the outfall at an arbitrary rate of 1 kg s⁻¹ (equivalent to a pollution load of 86,400 kg day⁻¹). Tidal current will then convey the pollutants and diluting it in the surrounding water. The mean pollutant elevation in Victoria Harbour due to the discharge of the new Kwun Tong nullah is shown in Figures 4A.1–4A.4.
- From the particle model result, the depth averaged pollutant elevation is reduced rapidly from the maximum of 57 mgL⁻¹ down to 5 mgL⁻¹, i.e. more than 10 times dilution, within approximately 500m from the outfall (Figures 4A.1–4A.2). The top 5m layer averaged pollutant elevation revealed a similar trend (Figures 4A.3–4A.4). In particular, the pollutant elevation under the proposed concrete decking at the mouth of YTB is $15 - 20 \text{ mgL}^{-1}$ and less than 5 mgL⁻¹ in Victoria Harbour. The maximum pollutant elevations at the <u>potentially</u> reprovisioned Cha Kwo Ling (NCKLSPS) and Yau Tong (NYTSPS) Saltwater Pumping Stations are 24.6 mgL⁻¹ and 11 mgL⁻¹ respectively.
- In order to estimate the actual increase in biochemical oxygen demand (BOD₅), SS, Ammoniacal Nitrogen and *E. Coli.*, the ratio between the actual pollution loads of each pollutant and the assumed load of 86,400 kg day⁻¹ is calculated. By assuming the same ratio between the actual and the modelled pollutant elevations in the neighbouring water, the actual pollutant elevation in Victoria Harbour can be estimated.
- 4 With reference to the modelled pollutant elevation and the effective loading at the new Kwun Tong Nullah outfall, the predicted increase in BOD₅, SS, Ammoniacal Nitrogen and *E. Coli*. are shown in Table 4A.1.

Modelled Pollutant Elevation ⁽¹⁾ [mgL ⁻¹]	BOD ₅ ⁽²⁾ [mgL ⁻¹]	SS ⁽²⁾ [mgL ⁻¹]	Ammoniacal Nitrogen ⁽²⁾ [mgL ⁻¹]	<i>E. Coli.</i> ⁽²⁾ [count per 100mL]
5	0	0.14	6.71 x 10 ⁻⁴	11
10	0.01	0.28	1.34 x 10 ⁻³	21
15	0.01	0.42	2.01 x 10 ⁻³	32
20	0.01	0.56	2.68 x 10 ⁻³	43
55	0.04	1.53	$7.38 \ge 10^{-3}$	118

Table 4A.1	Estimated	Pollutant	Elevation	due	to	the	New	Kwun	Tong	Nullah
	Discharge									

Note:

- 1. Modelled pollutant elevation corresponds to an arbitrary pollutant discharge rate of 1 kg s⁻¹ (86400 kg day⁻¹) at the outfall of the new Kwun Tong nullah.
- 2. Calculations were based on the effective loading at the outfall of the new Kwun Tong nullahas shown in Table 4.12, assuming 5% residual flows remain from expedient connections.
- 3. The results presented are based on the Full Reclamation option for YTB.
- 5 The distribution of averaged pollutant age in Victoria Harbour are shown in Figures 4A.5 to 4A.8. The result showed that the pollutants, discharging from the new Kwun Tong nullah outfall, will take an average time of 2 to 4 hours to be conveyed to and flushed out of the proposed concrete decking at YTB and into Victoria Harbour. This suggests that tidal flushing prevents the accumulation of pollutants under the decking and thus, unacceptable water quality is not expected.



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Modelled Pollutant Elevation ⁽¹⁾ [mgL ⁻¹]	$\frac{\text{BOD}_5}{[\text{mgL}^{-1}]}$	SS ⁽²⁾ [mgL ⁻¹]	Ammoniacal Nitrogen ⁽²⁾ [mgL ⁻¹]	E. Coli. ⁽²⁾ [count per 100mL]		
5	0	0.14	6.71 x 10 ⁻⁴	11		
10	0.01	0.28	1.34 x 10 ⁻³	21		
15	0.01	0.42	2.01 x 10 ⁻³	32		
20	0.01	0.56	2.68 x 10 ⁻³	43		
55	0.04	1.53	7.38 x 10 ⁻³	118		

Table 4A.1 Estimated Pollutant Elevation due to the New Kwun Tong Nullah Discharge

Note:

- Modelled pollutant elevation corresponds to an arbitrary pollutant discharge rate of 1 kg s⁻¹ (86400 kg day⁻¹) at the outfall of the new Kwun Tong nullah.
- Calculations were based on the effective loading at the outfall of the new Kwun Tong nullahas shown in Table 4.12, assuming 5% residual flows remain from expedient connections.
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